

Optical Structural Body, its Manufacturing Method and Optical
Element

This application is based on application Nos. 2002-263205
5 and 2003-85658 filed in Japan, the contents of which are
incorporated hereinto by reference.

BACKGROUND OF THE INVENTION

Field of the Invention

The present invention relates to an optical structural
10 body having a structure which can be applied to a polarizer,
a diffraction grading, a reflector, a filter, an optical
attenuator or the like to be used in the field of optical
communication and the like.

Description of the Related Art

15 A variety of structures have conventionally been proposed
for a polarizer to be used in an optical isolator or the like,
a diffraction grating to be used as an optical lens, and a
reflector, a filter or an optical attenuator to be used in a
spectroscope or the like.

20 To produce such conventional optical elements, however,
vacuum evaporation, sputtering, lithography or the like has
been used for forming a fine periodic structure in the submicron
order suited for integration of an optical circuit. This
disadvantageously not only complicates the production steps,
25 but also makes the equipment arrangement in a large scale,

resulting in increase in cost of the optical elements.

In view of the foregoing, it is an object of the present invention to provide an excellent optical structural body, its manufacturing method and an optical element in which production 5 can be conducted in an easy and quick manner, in which a fine periodic structure in the submicron order can readily be achieved, in which the direction, width and/or pitches of the fine periodic structure can optionally be controlled, and in which a three-dimensional periodic structure can be obtained.

10 BRIEF SUMMARY OF THE INVNETION

By condensing and irradiating, in a specific polarizing mode, pulse laser having a pulse width in the femtosecond order ($10^{-12} \sim 10^{-15}$ second) to the inside of a light transmitting substrate, a refractive-index changing region can be formed 15 only at the condensing position. This phenomenon that the refractive-index is changed by irradiating such femtosecond pulse laser, is called "a photoinduced change in refractive-index", and a formation of a light guide is known as an example.

20 The Inventor has discovered that there is formed, in the region presenting the photoinduced change in refractive-index, a periodic structure in which high refractive-index zones and low refractive-index zones are repeatedly being formed at pitches of $1 \mu\text{m}$ or less.

25 In the periodic structure, the planes in which the high

refractive-index zones or the low refractive-index zones are being joined to one another, are defined as "principal planes". It is noted that since the high refractive-index zones and the low refractive-index zones are adjacently alternately formed, 5 it is substantially the same whether the planes in which the high refractive-index zones are being joined to one another, are defined as "principal planes", or whether the planes in which the low refractive-index zones are being joined to one another, are defined as "principal planes". To make clear the 10 definition in the following description, however, the planes in which the high refractive-index zones are being joined to one another, are defined as "principal planes".

The principal planes are formed in parallel to the polarized magnetic field direction of the irradiated pulse 15 laser. Since the pulse laser is an electromagnetic wave, the pulse laser in its nature propagates while changing at predetermined oscillation frequency in the electric and magnetic fields with the electric and magnetic fields maintained in an orthogonal relationship. In this 20 specification, the direction of the magnetic field of the pulse laser is called a "polarized magnetic field direction".

The periodic structure is formed by interference of the irradiated pulse laser with plasma generated inside of the condensing position. Accordingly, the number of irradiated 25 pulse laser beams may be only one.

As conventionally reported, there is known an example in which at least two pulse laser beams to be irradiated are used to form a periodic structure by interference of these pulse laser beams with each other. According to the present invention, 5 however, the number of the pulse laser beams to be used is only one, thus extremely simplifying the equipment arrangement and the like.

It is a matter of course that pulse laser may be divided into at least two beams by a beam splitter or the like, or at 10 least two pulse laser beams may be used, such that these at least two beams are simultaneously irradiated to different parts of a light transmitting substrate. In such a case, there can be formed, inside of each pulse laser condensing position of the light transmitting substrate, a periodic structure in which 15 high refractive-index zones and low refractive-index zones are repeatedly being formed with predetermined pitches of, for example, 1 μm , or less.

The pitches in the periodic structure depend on the wavelength of the irradiated pulse laser, the number of 20 irradiated pulses or the pulse energy.

The periodic structure is formed by interference of the irradiated pulse laser with plasma generated inside of the condensing position. Accordingly, the following equation (1) is established from the law of conservation of momentum:

25
$$k_d = k_p - k_w \quad (1)$$

wherein k_w is the wave number vector of the pulse laser to be irradiated, k_p is the wave number vector of the plasma to be generated, and k_d is the modulated vector of repeat of the high refractive-index zones and the low refractive-index zones of 5 the periodic structure to be formed.

When it is now supposed that the wavelength of pulse laser to be irradiated is defined as λ , the equation of $k_w = 2\pi/\lambda$ is established. Further, when it is now supposed that the periodic structure pitches are defined as Λ , the equation of 10 $k_d = 2\pi/\Lambda$ is established.

Accordingly, when the wavelength λ of pulse laser to be irradiated is decreased, k_w is increased and k_d is decreased according to the equation (1). As a result, the pitches Λ in the periodic structure are increased.

15 The frequency ω_p in the longitudinal optical mode in plasma is expressed by the following equation (2):

$$\omega_p^2 = \frac{n_e e^2}{\epsilon_0 m_e} + \frac{3 \kappa_B T_e}{m_e} k_p^2 \quad . \quad (2)$$

wherein n_e is the electron density of the generated plasma, e is the electron charge of the generated plasma, ϵ_0 is the 20 dielectric constant of vacuum, m_e is the electron mass of the generated plasma, κ_B is the Boltzmann constant, and T_e is the

electron temperature of the generated plasma.

When the pulse energy and the irradiated pulse number of the pulse laser to be irradiated are increased, the electron density n_e of the generated plasma and the electron temperature T_e of the generated plasma are proportionally increased, and k_p is decreased. As a result, the modulated vector k_d of the periodic structure is decreased and the pitches Λ of the periodic structure are increased.

The power density of the pulse laser depends on the type 10 of the light transmitting substrate, but is preferably not less than 10^8W/cm^2 in order to form, inside of the condensing position, the periodic structure of the present invention in which high refractive-index zones and low refractive-index zones are repeatedly being formed with predetermined pitches or less.

15 The power density is a value obtained by dividing, by an irradiation unit area, the output power (W) of the pulse laser expressed in term of "the output energy peak value (J)/pulse width (second)". When the power density is smaller than 10^8W/cm^2 , there are instances where an effective periodic 20 structure is not formed inside of the condensing position. As the pulse energy is higher, the contrast between the high refractive-index zones and the low refractive-index zones becomes clearer (the difference in refractive-index becomes larger).

25 However, when a laser light having an excessively high

pulse energy amount is irradiated, a cavity defect is formed in the condensing position due to thermal effect. Accordingly, with the composition of the light transmitting substrate taken into consideration, the repetition frequency may be adjusted 5 such that the power density of the pulse laser is in the range between the threshold at which the periodic structure having pitches not greater than a predetermined value, e.g. 1 μ m, is formed inside of the condensing position, and the threshold at which a cavity defect is formed inside of the condensing 10 position. More specifically, also in view of the productivity, the lower limit of the repetition frequency of the pulse laser is set to 1 Hz, preferably set to 10 kHz, and more preferably set to 100 kHz, and the upper limit is set to 100 MHz. The pulse laser may be an optical pulse of a single shot.

15 Even with a high repetition-frequency pulse laser, a periodic structure having pitches of a predetermined value or less can be formed inside of the condensing position if there can be obtained a power density which causes a photoinduced change in refractive-index. On the contrary, even with a low 20 repetition-frequency pulse laser of 10 kHz or less, a periodic structure having pitches of a predetermined value or less can also be formed inside of the condensing position by adjusting, with the use of an ND (neutral density) filter or the like, the power density to not greater than the threshold at which a cavity 25 defect is formed.

In order that the pulse laser energy is adjusted between the threshold at which a periodic structure having pitches of a predetermined value or less is formed inside of the condensing position, and the threshold at which a cavity defect is formed, 5 and that there is formed a periodic structure in which the periodic pitches are uniform, in which the principal planes have the same width and are regularly aligned in the same direction, and in which the periodicity is excellent, it is preferable to adjust, in the range of $0.1 \mu\text{J}/\text{pulse}$ to $10 \mu\text{J}/\text{pulse}$, 10 the energy per pulse of the irradiated pulse laser, although this energy depends on the type of the light transmitting substrate.

Pulse laser is condensed by a condensing element such as a lens or the like. The region having the periodic structure 15 is basically spherical. While propagating in the light transmitting substrate, the pulse laser having a pulse energy causing a photoinduced change in refractive-index, is influenced by Kerr effect, i.e. a three-dimensional nonlinear optical effect. This causes the shape of the pulse laser 20 condensing position to be preferably spherical. The diameter of the sphere is preferably in a range from $0.1 \mu\text{m}$ to 1mm .

When this condensing position is continuously moved in a predetermined direction with respect to the light transmitting substrate, there can be formed an optical

structural body in which a region having the periodic structure extends in the form of a cord having a circular section or in the form of a column.

Further, when this condensing position is intermittently 5 moved in a predetermined direction at regular intervals with respect to the light transmitting substrate, there can be formed an optical element having so-called double periodic structures in which a plurality of spherical regions each having the periodic structure are repeatedly formed.

10 Further, when this condensing position is continuously moved in a predetermined direction at regular intervals with respect to the light transmitting substrate, there can be formed an optical element having so-called double periodic structures in which there are repeatedly formed a plurality of periodic 15 structures each in the form of a cord having a circular section or in the form of a column.

When such double periodic structures are three-dimensionally formed in a light transmitting substrate, a diffraction effect, a polarization effect, and a birefringent 20 effect can simultaneously be produced for a multiple-wavelength optical signal.

The birefringent effect is not generally produced in a glass material because of its isotropic structure. However, when there are formed periodic structures in which high 25 refractive-index zones and low refractive-index zones are

repeatedly being formed at pitches of a predetermined value or less, the birefringent effect can be given to an isotropic material even originally presenting no birefringent effect.

When light of wavelength division multiplex is incident
5 upon an optical element having double periodic structures in which there are repeatedly formed a plurality of periodic structures in which high refractive-index zones and low refractive-index zones are repeatedly being formed at pitches of a predetermined value or less, the reflectance of a specific
10 wavelength can be increased in dependence of the double periodic structures.

As discussed in the foregoing, according to the optical structural body of the present invention, there can be formed, inside of the condensing position, a periodic structure in which
15 high refractive-index zones and low refractive-index zones are repeatedly being formed at pitches of a predetermined value or less. This optical structural body can be formed at an optional position inside of a light transmitting substrate. When an optical signal in a predetermined wavelength range is incident
20 upon this optical structural body, a polarization effect, an interference effect and a diffraction effect can be produced.

Further, when the optical structural body of the present invention is formed in an isotropic light transmitting substrate which does not originally present a birefringence
25 phenomenon, a birefringent effect can be given to this optical

structural body, enabling the same to serve as a polarizer of an optical isolator or the like.

Further, when light of wavelength division multiplex is incident upon the optical structural body of the present 5 invention having double periodic structures, the reflectance of a specific wavelength in dependence on the periodic structure can be increased. Thus, this optical structural body serves as a reflector, a filter, or an optical attenuator which reflects light of a specific wavelength only.

10 An optical structural body manufacturing method according to the present invention utilizes interference of pulse laser condensed in a light transmitting substrate with plasma generated inside of the condensing position. Accordingly, merely by irradiating a single pulse laser beam 15 without subjecting to complicated processing steps, there can readily be produced an optical structural body having a periodic structure in which high refractive-index zones and low refractive-index zones are repeatedly being formed at pitches of a predetermined value or less.

20 The optical structural body of the present invention can be applied for a control element in the polarization direction of an optical signal to be used in optical communication, an optical element which produces a diffraction effect, and an optical element such as a reflector, a filter or an optical 25 attenuator which reflects an optical signal of a specific

wavelength.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a schematic view of apparatus for producing an optical structural body of the present invention;

5 Each of Fig. 2A to Fig 2C is a section view illustrating a periodic structure formed in a refractive-index changing region, wherein Fig. 2A is a front view in a light irradiation direction, Fig. 2B is a side view and Fig. 2C is a plan view;

10 Fig. 3A is a section view illustrating a periodic structure formed in a refractive-index changing region when there is irradiated pulse laser of which polarized magnetic field direction is horizontal;

15 Fig. 3B is a section view illustrating a periodic structure formed in a refractive-index changing region when there is irradiated pulse laser of which polarized magnetic field direction is vertical;

Fig. 5 is a perspective view of an example in which an optical structural body having double periodic structures is used as a diffraction grating or a polarizer;

20 Each of Fig. 4A to Fig. 4C is a section view illustrating a periodic structure formed in a refractive-index changing region, wherein Fig. 4A illustrates an example in which an optical signal of wavelength division multiplex is vertically irradiated onto the principal planes of the periodic structure 25 formed in the refractive-index changing region, Fig. 4B

illustrates an example in which an optical signal of wavelength division multiplex is irradiated, in a parallel manner, to the principal planes of the periodic structure formed in the refractive-index changing region, and Fig. 4C illustrates an 5 example in which an optical signal of wavelength division multiplex is vertically irradiated onto the principal planes of the periodic structure formed in the refractive-index changing region, and in which each pitch P in the periodic structure is larger.

10 Fig. 6 is a perspective view of an optical structural body having double periodic structures to be used as a reflector or a filter;

Fig. 7 is a perspective view of a quartz glass substrate to which pulse laser is being irradiated;

15 Fig. 8A is a perspective view of an optical structural body in which the condensing position has been intermittently moved in three directions at regular intervals with respect to the glass substrate to form a plurality of spherical refractive-index changing regions in the shape of a 20 three-dimensional lattice, and Fig. 8B is a plan view of Fig. 8A;

Fig. 9A is a perspective view of an optical structural body in which a plurality of column-like refractive-index changing regions are formed in a two-dimensional manner, and 25 Fig. 9B is a plan view of Fig. 9A;

Fig. 10 is a plan view of an optical structural body in which a plurality of refractive-index changing regions are formed in the shape of a triangle lattice; and

Fig. 11A is a perspective view of an optical structural body in which a plurality of column-like refractive-index changing regions are formed in a two-dimensional manner, and Fig. 11 B is a plan view of Fig. 11A.

DETAILED DESCRIPTION OF THE INVENTION

Fig. 1 is a schematic view of apparatus for producing an optical structural body of the present invention.

This optical structural body producing apparatus comprises an excitation light generating unit 3 for generating excitation light, a pulse light generating unit 4 for generating pulse laser based on the excitation light, and an optical amplifier 5 for amplifying the pulse laser.

The excitation light generating unit 3 is formed of a gas laser of Ar or the like, or a semiconductor laser of GaAs or the like.

The pulse light generating unit 4 is formed of a Ti:Al₂O₃ (titanium-doped sapphire crystal) laser. The Ti:Al₂O₃ laser is arranged to oscillate, by its mode lock mechanism, pulse light having a pulse width in the femtosecond order ($10^{-12} \sim 10^{-15}$ second). The wavelength of the pulse light is variable (100 nm ~ 2000 nm), but is for example set to 800 nm such that the pulse laser transmits a glass material 1.

The optical amplifier 5 is formed of a crystal solid laser such as Q switch Nd:YAG laser or the like.

Pulse laser supplied from the optical amplifier 5 is reflected by mirrors 9. Then, a linear polarized light is taken 5 out by a polarization plate 8 and condensed on the surface or inside of the glass material 1 by a condensing member 6 such as a lens or the like. The glass material 1 is disposed on an electrically-operated stage 7 capable of scanning in the X, Y, and Z directions.

10 The polarized light of pulse laser supplied from the optical amplifier 5 is generally a linear polarized light. However, when the polarization plate 8 is interposed in the optical path, the polarization can be aligned and the polarized angle can optionally be changed.

15 Examples of the glass material 1 to which pulse laser is to be irradiated, include glass materials such as oxide glass, halide glass, chalcogenide glass and the like, and crystal materials such as sapphire, crystal and the like. Examples of the oxide glass include glass of the silicate type, glass of 20 the borate type, glass of the phosphate type, glass of the phosphite type, glass of the bismuth type and the like. Examples of the halide glass include glass of the BeF_2 type, glass of the ZrF_4 type, glass of the InF_3 type, glass of the Cd-Zn-Cl type and the like. Examples of sulfide glass include 25 glass of the Ga-La-S type and the like. Examples of the

chalcogenide glass include glass of the S-As type and the like.

Pulse laser having power density of 10^8W/cm^2 or more is condensed at the condensing position on the surface or inside of the glass material 1. This causes a phenomenon of 5 photoinduced change in refractive-index to be generated inside of the condensing position. This results in formation of a substantially spherical refractive-index changing region. The size of the refractive-index changing region is defined by the capacity of the condensing member 6, the pulse laser 10 wavelength and the pulse energy, but is generally in the range of 1 μm to 1 mm.

Further formed inside of the refractive-index changing region is a periodic structure in which high refractive-index zones and low refractive-index zones are being repeatedly 15 formed at pitches of 1 μm or less (submicron).

Each of Fig. 2A to Fig 2C is a section view illustrating a periodic structure formed in a refractive-index changing region.

High refractive-index zones 17 and low refractive-index 20 zones 18 are periodically alternately formed in the refractive-index changing region S. Each periodic pitch is expressed by P, and the width of each high refractive-index zone 17 is expressed by L. These pitch P and width L are dependent on the polarization direction of the pulse laser to be

irradiated, the wavelength, the number of the irradiated pulses, the pulse energy and the like. Accordingly, by setting these values as variables, there can be prepared a periodic structure suitable for an optical signal of an optional wavelength range.

5 Fig. 2A shows a periodic structure prepared by irradiating, vertically to the paper plane, pulse laser of which magnetic field polarization direction is horizontal. In the periodic structure formed in the spherical refractive-index changing region S (of which diameter is expressed by D), the 10 planes (principal planes) in which the high refractive-index zones 17 are joined to one another, are formed in round slices in parallel to the magnetic field polarization direction.

Fig. 2B shows a periodic structure prepared by irradiating pulse laser horizontally from the right hand of the 15 paper plane. The pulse laser light is vertical to the paper plane.

Fig. 2C shows a periodic structure prepared by irradiating pulse laser light upwardly from the lower part of the paper plane.

20 Fig. 3A and Fig. 3B show the relationship between the principal plane forming direction and the pulse laser polarization. Fig. 3A shows a periodic structure prepared by irradiating, vertically to the paper plane, pulse laser of which magnetic field polarization direction is horizontal. Fig. 3B 25 shows a periodic structure prepared by irradiating, vertically

to the paper plane, pulse laser of which magnetic field polarization direction is vertical. Thus, the direction of the principal planes formed by the high refractive-index zones 17, is identical with the polarized magnetic field direction.

5 According to the present invention having the arrangement above-mentioned, a periodic structure in which the refractive-index is changed in the submicron order, can be formed in the refractive-index changing region. The periodic direction of the periodic structure can be set in an optional 10 direction by setting the polarized magnetic field direction of the pulse laser to be irradiated.

Fig. 4A to Fig. 4C are section views illustrating the structures of refractive-index changing regions formed by setting the polarization direction of pulse laser to be 15 irradiated, the wavelength, the number of irradiated pulses, the pulse energy and the like, these structures being different in principal plane direction and in pitch P in the periodic structures from one another.

In the refractive-index changing region S in Fig. 4A, the 20 principal plane direction is horizontal. A signal light of wavelength division multiplex is vertically incident upon the principal planes. In the refractive-index changing region S in Fig. 4B, the periodic pitches P are the same as in Fig. 4A, but the principal plane direction is vertical. A signal light 25 of wavelength division multiplex is incident upon the principal

planes in parallel thereto. Fig. 4C shows the structure in which a signal light of wavelength division division multiplex is vertically incident upon the principal planes as done in Fig. 4A, but the periodic pitches P are different from those in Fig. 5 4A.

By a difference in the incident angle of signal light of wavelength division multiplex and a difference in pitch P , it can be expected to increase the reflectance of a specific wavelength in dependence on the incident angle upon the 10 principal planes and the pitches P . More specifically, a reflected light A reflected in Fig. 4A, a reflected light B reflected in Fig. 4B, and a reflected light C reflected in Fig. 4C, are different in wavelength from one another.

In the foregoing, the description has been made of the 15 case in which a single refractive-index changing region is formed. However, a plurality of refractive-index changing regions may be formed. Further, the shape of the refractive-index changing region is not limited to a spherical shape.

20 In Fig. 1, after laser light has been irradiated to the glass material 1, the laser light is turned off. Then, the glass material is moved by a predetermined distance in the X, Y and Z directions, and laser light is irradiated again to the glass material 1. When such operations are repeated, there can be 25 discretely repeatedly formed, on the surface or inside of the

glass material 1, a plurality of spherical refractive-index changing regions each having the periodic structure above-mentioned.

By continuously moving, by a predetermined distance in 5 the X, Y and Z directions, the glass material under irradiation by laser light, a refractive-index changing region having the periodic structure can be formed on the surface or inside of the glass material in the shape of a column or a curved cord having a circular section.

10 Further, the glass material 1 under irradiation by laser light, is continuously moved in one direction selected from the X, Y and Z directions. After the movement is finished, the laser light is turned off and the glass material 1 is intermittently moved by a predetermined distance in other direction. Then, 15 the laser light is again turned on and the glass material 1 is continuously moved in the one direction. When such operations are repeated, a plurality of column-like refractive-index changing regions can repeatedly be formed on the surface or inside of the glass material 1.

20 Further, the glass material 1 is continuously moved in a manner of a curved line in an optional direction. After the movement is finished, the laser light is turned off. Then, the glass material 1 is intermittently moved by a predetermined distance in other direction. The laser light is again turned 25 on and the glass material 1 is moved in a manner of a curved

line. When such operations are repeated, there can repeatedly be formed, on the surface or inside of the glass material 1, a plurality of refractive-index changing regions each in the shape of a curved cord having a circular section.

5 Thus, when a plurality of refractive-index changing regions are formed at regular intervals in a predetermined direction, there can be formed, at an optional position in the glass material, an optical structural body in which the refractive-index changes in a double periodic manner. The 10 predetermined intervals may be for example in the range of 1 μm to 1 mm.

When an optical signal of optional wavelength and optional polarization is incident upon an optical structural body having such double periodic structures as shown in Fig. 15 5, it is possible to expect that this optical structural body produces the effect of a diffraction grating or a polarizer which not only diffracts the optical signal in a predetermined direction per wavelength, but also takes out an optical signal of predetermined polarization. Further, a combination of two 20 polarizers having the arrangement above-mentioned and a Faraday rotor held therebetween, can serve as an optical isolator.

When the optical structural body has a three-dimensionally layered arrangement with the directions and pitches of the principal planes of the periodic structures changed in 25 each layer as shown in Fig. 6, this optical structural body can

be applied for a reflector or a filter for reflecting, with high efficiency, only an optical signal of a specific wavelength from the optical signal of wavelength division multiplex.

The embodiments above-mentioned are shown only by way of 5 examples, and the present invention may suitably be embodied in different manners without departing from the scope of the present invention.

[Example 1]

A plurality of refractive-index changing regions were 10 repeatedly formed in a quartz glass substrate 10 of 10 mm x 10 mm x 5 mm. As shown in Fig. 7, pulse laser 11 was condensed by a lens 12 and irradiated to the quartz glass substrate 10 such that the condensing position 13 of the pulse laser 11 was located inside of the quartz glass substrate 10. Used as the 15 pulse laser was laser which was oscillated from Ti:Al₂O₃ laser excited by argon laser, of which pulse width was 150 femtoseconds, of which repetition frequency was 200 kHz, of which wavelength was 800 nm, of which average output was 600 mW, and of which polarized magnetic field is horizontal. The 20 irradiation period of time was 4 seconds for one condensing position.

Formed in the condensing position 13 was a striped periodic structure in which first and second zones different in refractive-index from each other were formed at pitches of 25 1 μ m or less.

The diameter of the refractive-index changing region having the periodic structure thus formed, was about 2 μm , the pitches P in the periodic structure were 200 nm, the width L of the first zone was about 30 nm, and the width of the second 5 zone was about 170 nm.

The first zone including an oxygen defect was changed to a composition SiO_{2-x} ($0 < x < 2$). It is therefore considered that its refractive-index is higher than the ambient refractive-index (the refractive-index of the glass substrate 10 except for the periodic structure). From the first zone, oxygen was moved to the second zone and taken in the structure thereof, causing the second zone to be changed to a composition SiO_{2+x} . It is therefore considered that its refractive-index is substantially equal to or less than the ambient 15 refractive-index (the refractive-index of the glass substrate except for the periodic structure). However, it can be considered that as oxygen is decreased in amount, the refractive-index is lowered, and that as oxygen is increased in amount, the refractive-index is increased. Accordingly, 20 the relationship between oxygen and refractive-index cannot definitely be determined at the present stage. However, it is true that the first and second zones undergo a change in refractive-index.

The size D of the refractive-index changing region is

variable in the range of about 1 μm to about 100 μm dependent on the pulse energy of the pulse laser to be irradiated and the magnification of the lens used for light collection. Dependent on the wavelength of pulse laser to be irradiated, the number 5 of irradiated pulses, the pulse energy and the refractive-index of the glass substrate, the width L of the first zone is variable in the range of about 10 to about 50 nm and the width of the second zone is variable in the range of about 50 to about 190 nm.

10 When the condensing position 13 is intermittently moved at predetermined intervals in the X, Y and Z directions with respect to the inside of the quartz glass substrate 10 (the irradiation period of time is 4 seconds for one condensing position), spherical refractive-index changing zones 14 are 15 repeatedly formed as shown Fig. 8A. Fig. 8B is a plan view of the quartz glass substrate 10 in which these refractive-index changing zones 14 are repeatedly being formed.

When the pulse laser 11 is intermittently moved in the X and Y directions, and continuously moved in the Z direction 20 with respect to the inside of a quartz glass substrate (the Z-directional moving speed is 100 $\mu\text{m/sec.}$), column-like refractive-index changing zones 15 are repeatedly formed as shown Fig. 9A. Fig. 9B is a plan view of the quartz glass substrate 10 in which such column-like refractive-index

changing zones 15 are being repeatedly formed.

Further, when the pulse laser 11 is intermittently moved in the direction at 60° from the X direction (30° from the Y direction) and is continuously moved in the Z direction at the 5 speed above-mentioned with respect to a quartz glass substrate 10, there can be formed, in the quartz glass substrate 10, column-like refractive-index changing zones 15 generally in the shape of a triangle grating as shown in Fig. 10.

When the pulse laser 11 is intermittently moved in the 10 X direction and is continuously moved in the Y direction (at the speed of $100 \mu \text{m/sec}$), there are formed column-like refractive-index changing zones 16 as shown in Fig. 11A. Fig. 11B is a plan view of the quartz glass substrate 10 in which the column-like refractive-index changing zones 16 are 15 repeatedly being formed.

[Example 2]

As done in Example 1, pulse laser 11 was irradiated to a quartz glass substrate 10 of $10 \text{ mm} \times 10 \text{ mm} \times 5 \text{ mm}$ such that the condensing position of the pulse laser 11 was located inside 20 of the quartz glass substrate 10. The pulse laser irradiation conditions were the same as those used in Example 1.

In Example 2, the pulse laser was irradiated with its polarization direction (magnetic field) changed to horizontal or vertical by the linear polarization plate 8 in Fig. 1.

As shown in Fig. 3A and Fig. 3B, there was formed, in the direction in dependence on the pulse laser light polarization direction (magnetic field), a striped periodic structure in which high refractive-index zones and low refractive-index 5 zones were being repeatedly formed. More specifically, a transversely striped periodic structure was formed when the polarization direction is horizontal (Fig. 3A), and a longitudinally striped periodic structure was formed when the polarization direction is vertical (Fig. 3B).

10 As in Example 1, the condensing position was intermittently or continuously moved in a predetermined direction at regular intervals with respect to a glass substrate, thereby to repeatedly form spherical or column-like refractive-index changing regions, or refractive-index 15 changing regions each in the shape of a cord having a circular section.